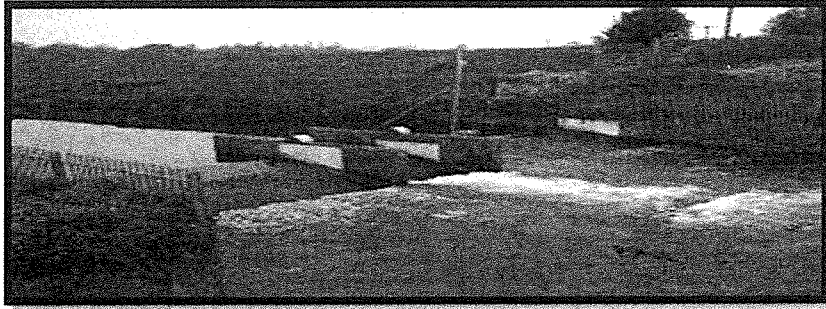


# ***DESIGN OF IRRIGATION STRUCTURE (2)***

[engineer22.com](http://engineer22.com)

رابعة مدني



## **Regulator (Gate lifting structure) a- Part (1)**

6

# Gate Lifting structure

قبل تصميم أى حاجت لابد من تحديد نوع البوابة :-

$$\therefore A_g = B_g * H_g$$

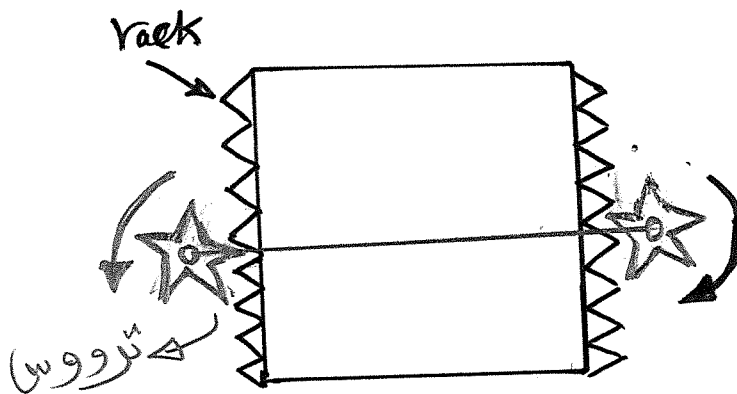
$$A_g \leq 16 \text{ m}^2 \rightarrow \text{single gate}$$

$$A_g > 16 \text{ m}^2 \rightarrow \text{Double gate}$$

\* بعد تصميم ال gate سنبداً في تصميم منشأ رفع البوابات (gate lifting structure) ولكن لاحظ الاتى :-

\* For single gate :-

في حالة البوابة واحدة يتبع رفع البوابة بالنظام الاتى :-  
(Fahmy Henein type)



(Fahmy Henein gate)

ولانحتاج منشأ رفع البوابات (gate lifting structure)

وانها يتبع استضافة في ال (Double gate)

فقط

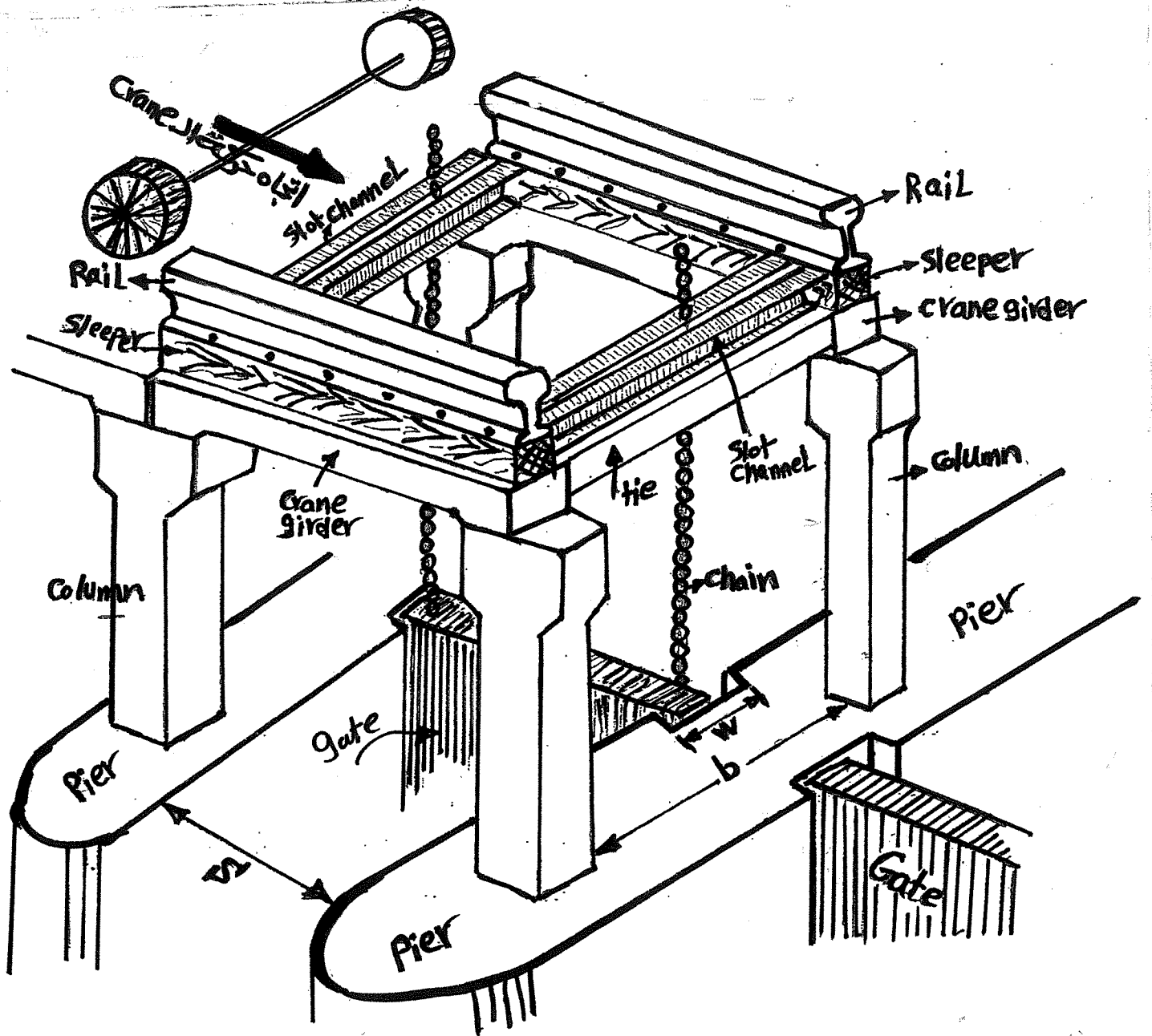
## For Double gates

- يتم استخدام ونش (Crane) لرفع البوابة وبدلاً من عمل ونش لكل فتحة من فتحات القناطر يتم عمل نظام لتحريك النش بين الفتحات .

- يتم وضع عمودين (2 Columns) على كل Pier ويرتكز عليهما كمرّة رئيسيّة خرسانيّة (Crane girders) ويتم وضع القضبان (Rails) التي سيتحرك عليها النش .  
- طقاومة الاهتزازات الناتجة من حركة النش يتم وضع كمرّة خرسانيّة (Tie) بين كل عمودين في الاتجاه العرضي .

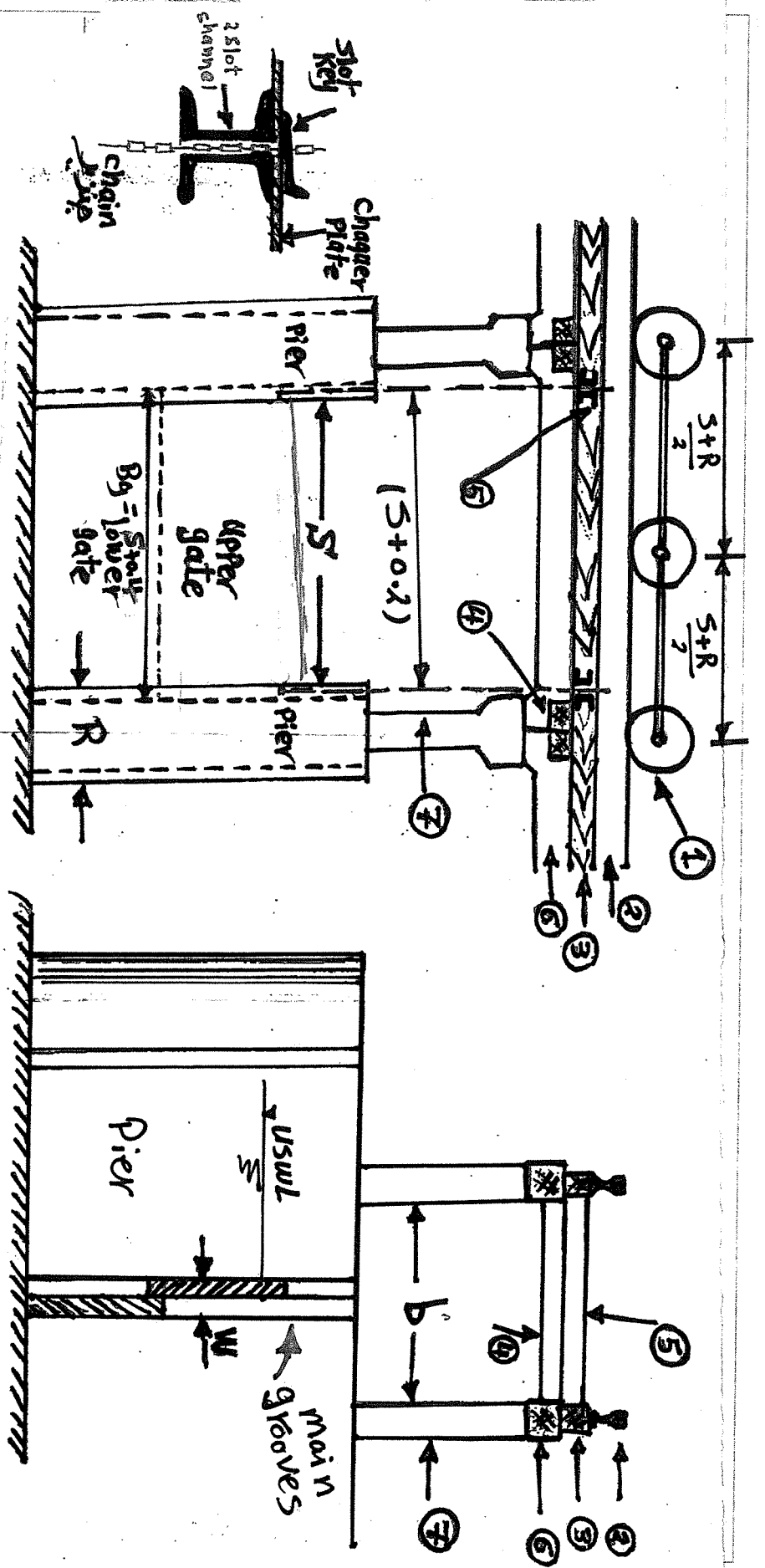
تعالوا نشوف شكل  
(gate lifting structure)

# مكونات (Gate lifting structure)



# المكونات

- 1- Crane الوخشي
- 2- Rail
- 3- sleeper الفلنك
- 4- Tie
- 5- 2 slot channel
- 6- Crane girder
- 7- Column



( See 5.v )

See ( ELEV )

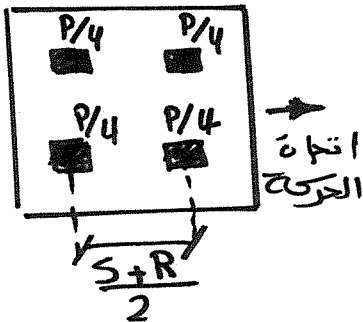


S (m)	b (m)	W (m)
3	1.0	0.6
4	1.0	0.75
5	1.25	0.9
6	1.5	1.0
8	1.8	1.2

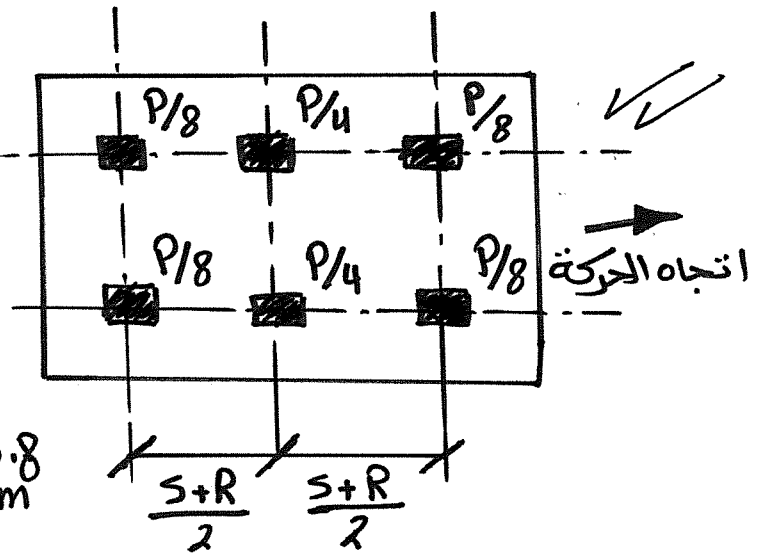
# Design of Gate lifting structure

## 1- Crane :-

if  $S \leq 4m$   
4 (wheel)



if  $S > 4m$   
6 (wheel)



$$\therefore R = \frac{S}{5-8} \times 0.8 \text{ m}$$

عرض  
Pier  $R_c$

\* يرتكز الونش على 6 عجلات .

\* البعد بين كل عجلتين في اتجاه الحركة هو  $(\frac{S+R}{2})$  بحيث يكون

الونش فوق الفتحة تماماً في حالة رفع البواب.

\* وزن الونش كله (P) وهو يساوي عرض  
الفتحة S

$$P = S (\text{ton})$$

example if  $S = 5 \text{ m}$   $\therefore P = 5 \text{ ton}$

$S = 6 \text{ m}$   $\therefore P = 6 \text{ ton}$

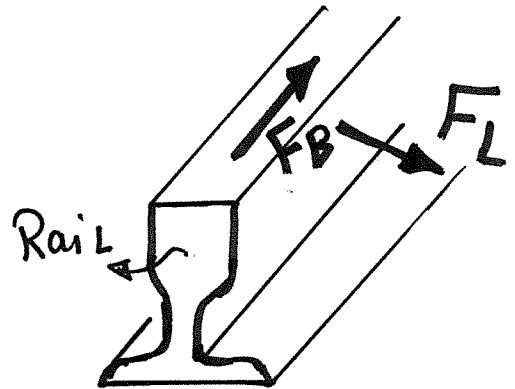
\* ويوجد Impact نتيجة حركة الونش بمقدار (I) بحيث

$$I = 0.2$$

\* وحسب القوى الاتية ا-

\*  $F_B = \text{Braking Force}$   
القوة الناتجة من الفرمل

$$F_B = \frac{P}{7}$$



\*  $F_L = \text{Lateral Force}$   
القوة الناتجة عن اهتزازات الونش

$$F_L = \frac{P}{4}$$

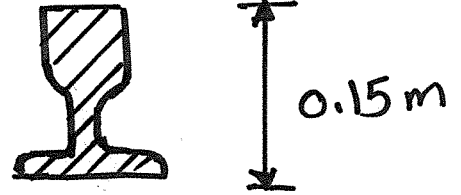
## 2- Rail :- القضبان

$$\text{height} = 0.15 \text{ m}$$

$$\text{own wt} = 0.05 \text{ t/m}^1$$

وزن Rail

(حقت)

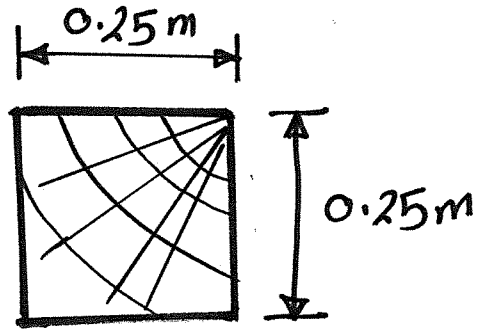


## 3. Sleeper :- الفلنكات

تكون من الخشب وابعادها

$$(0.25 \text{ m} * 0.25 \text{ m})$$

حقت



$$\gamma_{\text{wood}} = 0.9 \text{ t/m}^3$$

$$\text{own wt} = (0.25 * 0.25) * \gamma = \nu \text{ t/m}^1$$

وزن الفلنكة



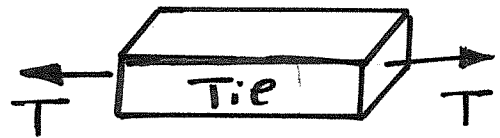
# 4 - Tie :-

الشداد

هي كمره خرسانية تتحمل القوى الجانبية  $F_L$

$$\therefore T = \frac{F_L}{2} = \frac{P/4}{2} = \frac{S}{8}$$

← لوجود شتارين في نفس الباكيت



$\therefore T_0 \rightarrow$  Design Force

$$T_0 = T * (F.o.S) / 4$$

← معامل امان  
دياخذ 4

∴ من الآخر

$$T_0 = \frac{S}{2} = \frac{P}{2}$$

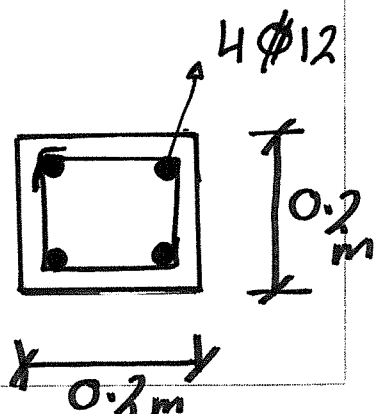
Design

$$A_s = \frac{T_0 * 10^3}{f_s} = \checkmark \text{ cm}^2$$

∴ الفس

$$\therefore f_s = 1200 \text{ kg/cm}^2$$

Using min steel  $4 \phi 12$   $A_{smin}$



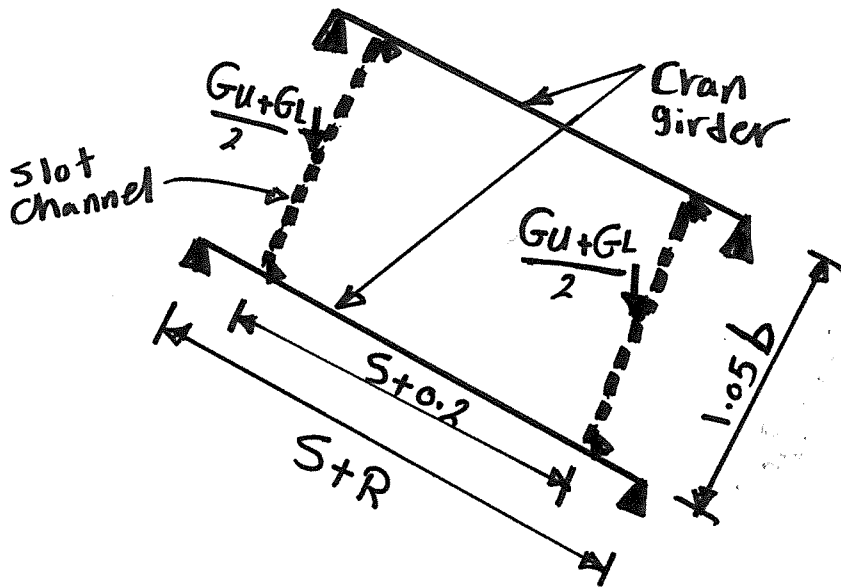
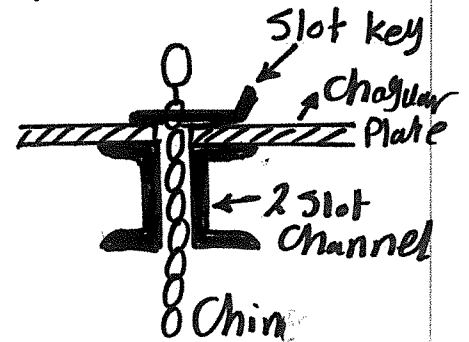
# 5- Slot Channel:-



هو عبارة عن كمرتين UPN (C) مركبة على (Cran girder)

\* اسوا حاله لتجهيز (2 slot channel) عندما تكون

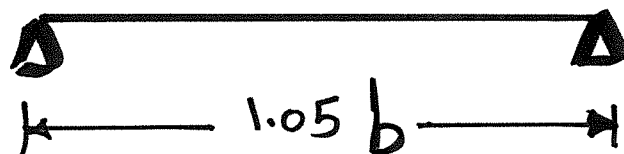
البوابتين معلقتين



وظيفة (2 slot channel) هو تعليق البوابات السطحية والعلوية.

\* structure system :-

من جدول  $b$   
على حسب  $S$



# Loads

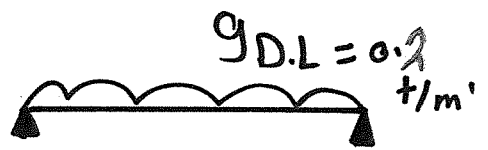
## a- Dead Load

$$g_{D.L} = \text{own wt} + (\text{Chaquor Plate} + L.L)$$

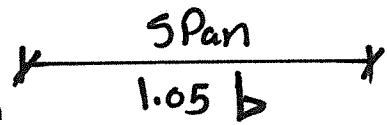
$$g_{D.L} = 0.05 + 0.15 = 0.2 \text{ t/m}$$

(Chaquor) ← نواع

$$\therefore M_{D.L} = \frac{g_{D.L} * S_{\text{Pan}}^2}{8} = \text{t.m}$$



$$\therefore Q_{D.L} = \frac{g_{D.L} * S_{\text{Pan}}}{2} = \text{ton}$$

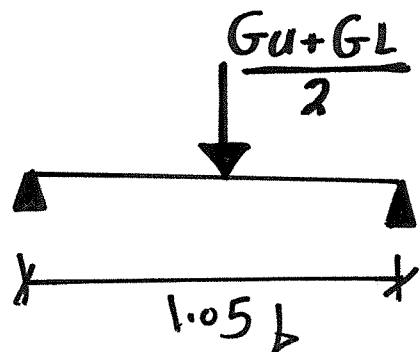


## b- Live Load

$$\therefore G_U = G_L \quad \text{وزن البوابة}$$

upper      lower

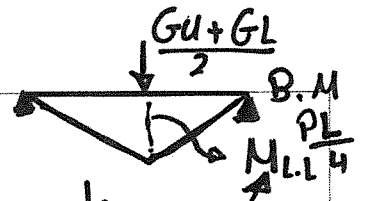
$$G_U = A_g * g$$



$$\therefore g = 0.06 * S$$

$$A_1 g = B_g * H_1 g$$

$$\therefore M_{L.L} = \frac{\left(\frac{G_u + G_L}{2}\right) * \text{Span}}{4} = \nu \nu \text{ t.m}$$



$$\therefore Q_{L.L} = \frac{\left(\frac{G_u + G_L}{2}\right)}{2} = \frac{G_u + G_L}{4}$$

$$\therefore M_t = M_{D.L} + M_{L.L} = \nu \nu \text{ t.m}$$

$$Q_t = Q_{D.L} + Q_{L.L} = \nu \nu \text{ ton}$$

Design

$$Z_{2E} = \frac{M_t * 10^5}{f_y (1200)} = \nu \nu \text{ cm}^3$$

$$Z_{1E} = \frac{Z_{2E}}{2} = \nu \nu \text{ cm}^3$$

يق اختيار القطع من جدول (UPN)

Check of shear

$$q = \frac{Q_t * 10^3}{2 t_w * h_w} = \nu \nu \neq q_{all} \quad \text{ok}$$

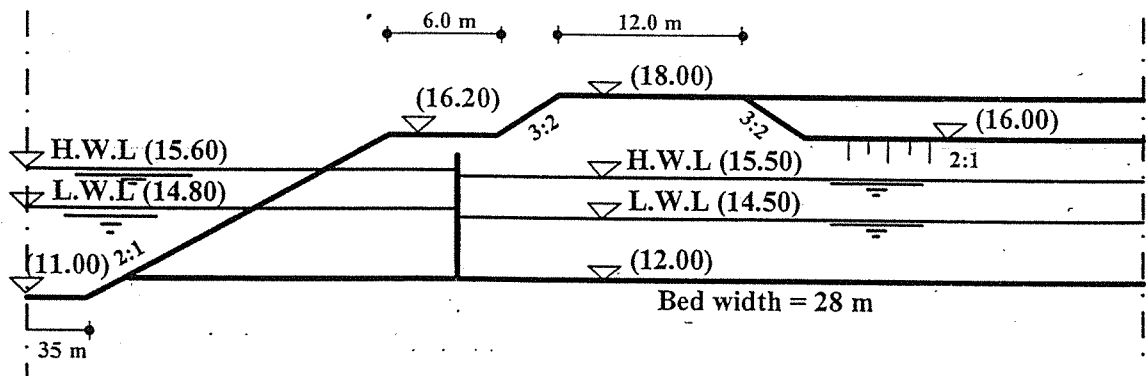
### Regulators & Barrages

A reinforced concrete **head regulator** is to be constructed to feed a main canal from a Rayah. A longitudinal dimensioned section through the main canal at the regulator site is given in the figure. The available data for the regulator are:

- The regulator consists of four vents of 6.0 m span for each,
- The maximum allowable discharge through the main canal is 7.5 million  $m^3/d$ ,
- The bridge width over the regulator is 12.0 m and it has two sidewalks of 1.50 m width for each,
- The equivalent D.L of the bridge, L.L on the traffic lanes, and L.L on the sidewalks are 2.0, 1.0, 0.4  $t/m^2$ , respectively,
- The soil properties at the regulator site are:  $\Phi = 30^\circ$ ,  $\gamma_{bulk} = 1.65 t/m^3$ , and the allowable bearing capacity is 1.50  $kg/cm^2$ , and
- Sliding vertical steel gates with horizontal main girders are used.

It is required to:

- ✓ 1. Check the hydraulic design of the regulator,
- ✓ 2. Give the complete structural design for each of the following elements:
  - ✓ • The sliding gates and find the required lifting force,
  - ✓ • The required R.C gate lifting structure,
    - The R.C piers, and
    - The R.C floor, considering the required lengths for percolation and scouring;  $C_B = 12$ .
3. Draw neat sketches showing the following:
  - i. Plan (H.E.R)
  - ii. Longitudinal section through the regulator



# Given

\* Head Regulator

\*  $N = 4$

\*  $S = 6 \text{ m}$

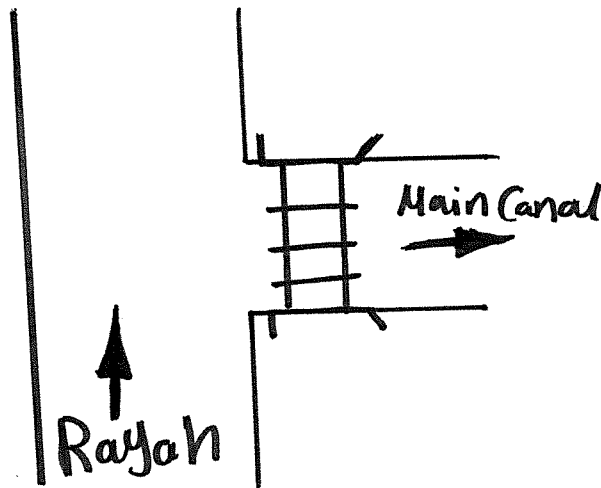
$$* Q = 7.5 \times 10^6 \text{ m}^3/\text{day} = \frac{7.5 \times 10^6}{24 \times 60 \times 60} = 86.8 \text{ m}^3/\text{sec}$$

\* check of hydraulic Design :

\* خلی بالی صحتی  $S$  و  $N$  وکن نعل

check علی  $\alpha$  واد  $V_r$

\* خلی بالی ال (Head regulator) یکون فی بدایت  
التریح ال اصغر درجت .

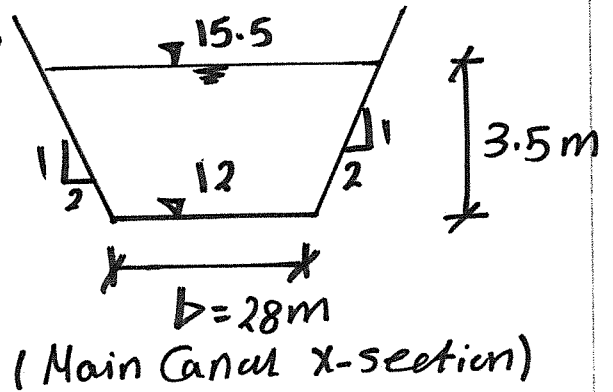


$$A_{ds} = (b + y_{ds} Z) y_{ds}$$

$$A_{ds} = (28 + 3.5 \times 2) \times 3.5 = 122.5 \text{ m}^2$$

$$\therefore A_{ww} = N \times S \times y_{ds}$$

$$A_{ww} = 4 \times 6 \times 3.5 = 84 \text{ m}^2$$



$$* V_r = \frac{Q}{A_{ww}} = \frac{86.8}{84} = 1.03 \text{ m/sec}$$

$$1.0 < V_r < 2.0$$

OK

يمكن السرعة نقل عن 1 على

$$* B_{eact} = N \times S = 6 \times 4 = 24 \text{ m}$$

$$B_{e2} \geq 0.5 \frac{A_{ds}}{y_{ds}}$$

$$B_{e2} \geq 0.5 \frac{122.5}{3.5} = 17.5 \text{ m}$$

$$\therefore B_{eact} > 17.5 \text{ m}$$

24 m

OK

شروط

## check of heating up

$$h_{up} = \frac{v_{us}^2}{2g C^2} \left( \left( \frac{A_{us}}{A_{ww}} \right)^2 - 1 \right) \neq h_{all}$$

$$A_{us} = (b + y_{us} Z) y_{us}$$

$$y_{us} = y_{Ds} + 0.1 = 3.5 + 0.1 = 3.6 \text{ m}$$

$$\rightarrow A_{us} = (28 + 3.6 \times 2) 3.6 = 126.72 \text{ m}^2$$

$$\rightarrow v_{us} = \frac{Q}{A_{us}} = \frac{86.8}{126.72} = 0.684 \text{ m/sec}$$

$$\rightarrow \therefore S > 4 \quad \therefore C = 0.92$$

$$\rightarrow A_{ww} = 84 \text{ m}^2$$

$$h_{up} = \frac{(0.684)^2}{2 \times 9.81 \times (0.92)^2} \left( \left( \frac{126.72}{84} \right)^2 - 1 \right) = 0.035 \text{ m}$$

$$h_{up} = 3.5 \text{ cm} < 10 \text{ cm ok}$$



2- Given the Complete structural Design for each:

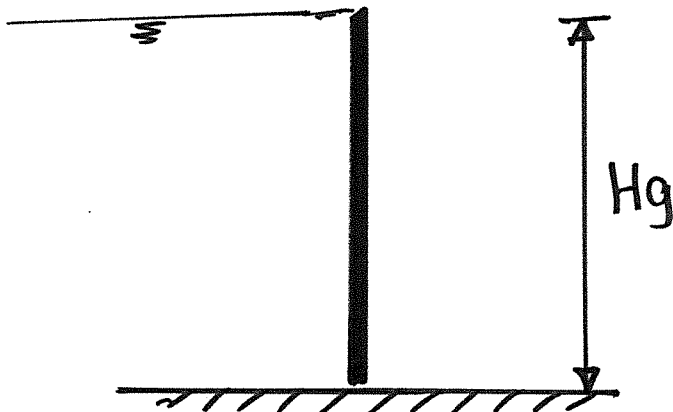
- The steel Sliding gates and Find the required Lifting Force?

الحل

$$S = 6 \text{ m}$$

$$y_{us} = y_{ds} + h_u = 3.5 + 0.1 = 3.6 \text{ m}$$

\* تحديد نوع البوابة



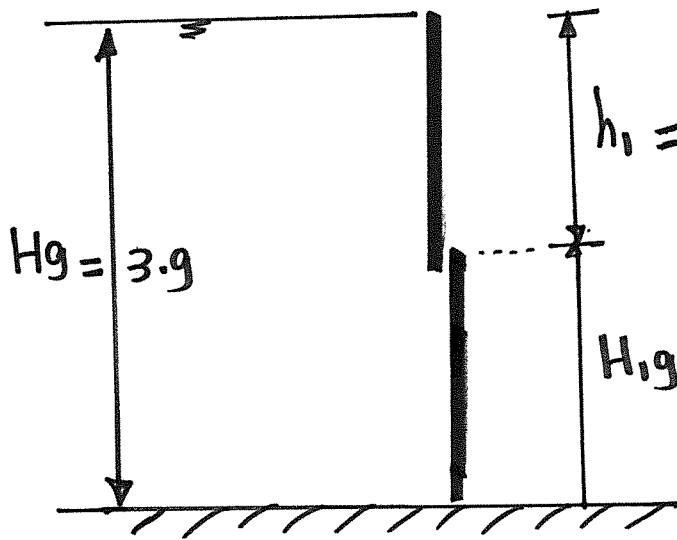
$$H_g = y_{us} + 0.3 = 3.6 + 0.3 = 3.9 \text{ m}$$

$$B_g = S + 0.4 = 6 + 0.4 = 6.4 \text{ m}$$

$$\therefore A_g = H_g \times B_g = 3.9 \times 6.4 = 24.96 > 16 \text{ m}^2$$

Double gate

\* تحديد ابعاد البوابة



$$B_g = 5 + 0.4 = 6.4 \text{ m}$$

$$H_{1g} = \frac{H_g}{2} + 0.1$$

$$H_{1g} = \frac{3.9}{2} + 0.1 = 2.05 \text{ m}$$

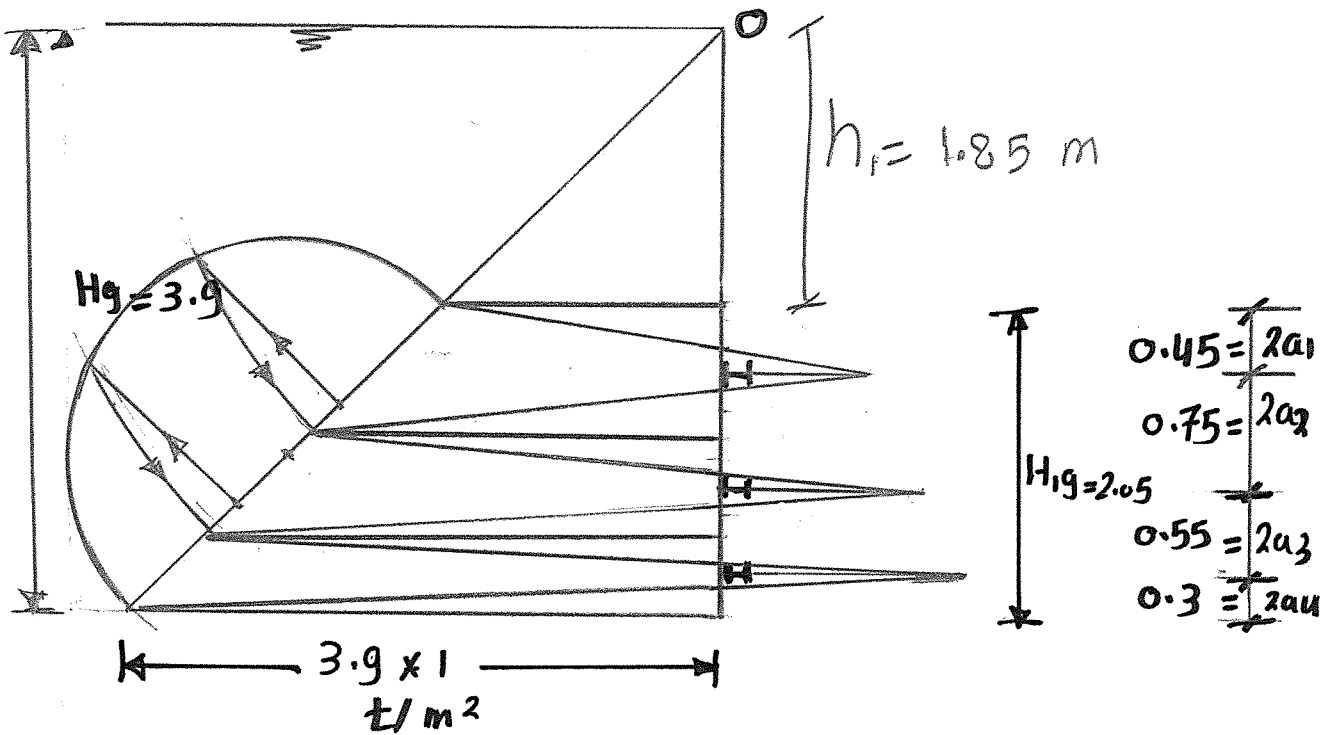
Used Double gate of Dimension

( 6.4 × 2.05 ) For each gate

# Location of MG

4MG و 3MG يتبع فرضها لدریغها عدد MG

assume  $N_{MG} = 3MG$



ولازم نتاكر ان

$$2a_1 + 2a_2 + 2a_3 + 2a_4 = H_g = 2.05 \text{ m}$$

# Design of skin Plate

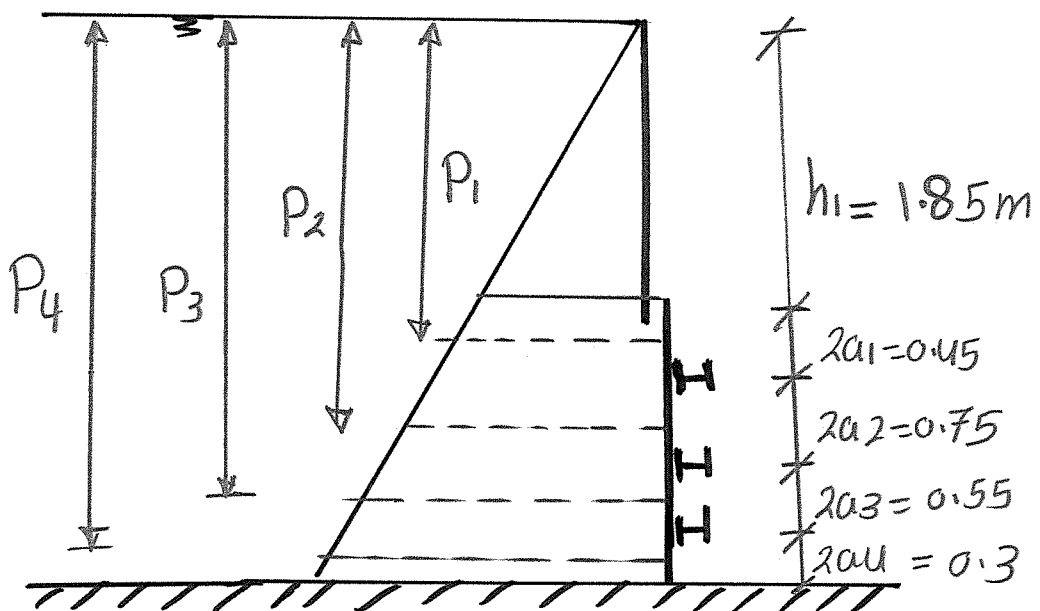
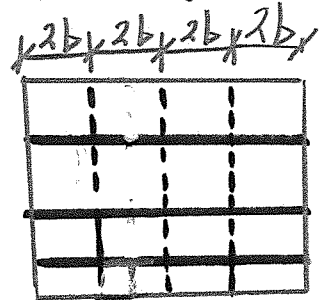
No of XG <sup>فرض</sup> assume = 3 XG

$$2b = \frac{BG}{\frac{(N_{XG} + 1)}{3}} = \frac{6.4}{4} = 1.6 \text{ m}$$

$$\therefore t(\text{cm}) = a * b * \sqrt{\frac{2 * M * P}{f(a^2 + b^2)}}$$

$$f = 1 \text{ t/cm}^2$$

$$m = 0.94$$



No	$a_{(m)}$	$b_{(m)}$	$P$ ( $t/m^2$ )	$t$ (cm)
1	0.225	0.8	$1 * (1.85 + 0.225) = 2.075$	0.43
2	0.375	0.8	$1 * (1.85 + 0.45 + 0.375) = 2.675$	0.761
3	0.275	0.8	$1 * (1.85 + 0.45 + 0.75 + 0.275) = 3.325$	0.65
4	0.15	0.8	$1 * (1.85 + 0.45 + 0.75 + 0.55 + 0.15) \cdot$ $= 3.75$	0.39

$$t_{\text{Max}} = 0.761 \text{ cm} < 1 \text{ cm}$$

Take  $\therefore t = 1 \text{ cm}$

---

# Design of XG

نفس الارقام من Skin Plate

$\frac{2}{3} P * 2a$

$\frac{1}{2} * P * 2a$

$\frac{P_4 * s_{Pan}}{8}$

$\frac{P_5 * s_{Pan}}{2}$

No	sPan 2a	P (t/m <sup>2</sup> )	P <sub>4</sub> (t/m)	P <sub>5</sub> (t/m)	M (t.m)	Q (t)
1	0.45	2.075	0.62	0.467	0.015	0.105
2	0.75	2.675	1.337	1.003	0.094	0.375
3	0.55	3.325	1.22	0.914	0.046	0.251
4	0.3	3.75	0.75	0.56	0.008	0.084

$M_{max} = 0.094 \text{ t.m}$  (  $Q_{max} = 0.375 \text{ ton}$  )

$$Z_{req} = \frac{M \times 10^5}{1000} = \frac{0.094 \times 10^5}{1000} = 9.4 \text{ cm}^2$$

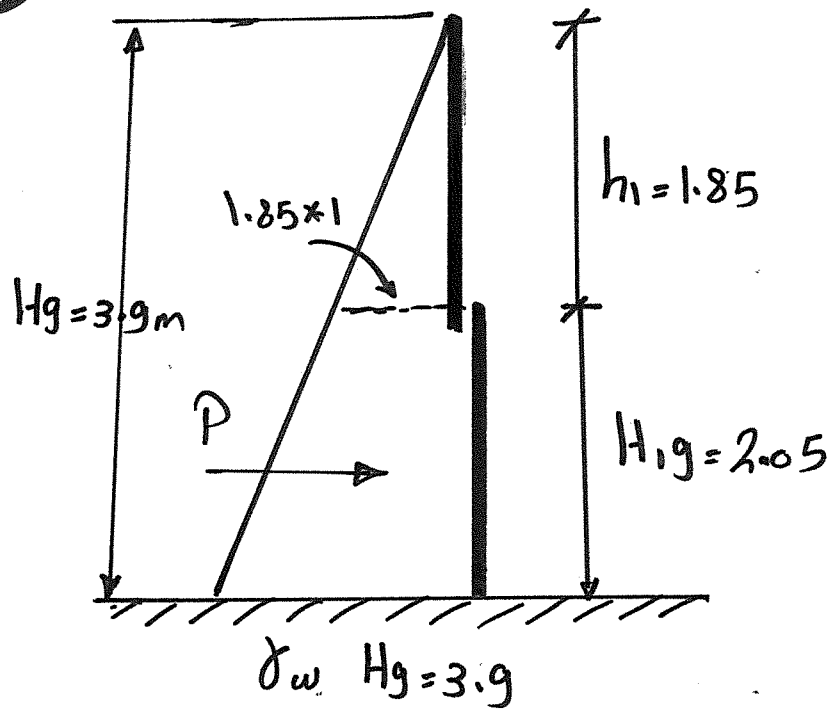
Use S I B  $N_0 = \checkmark$

## Check of shear

$$q = \frac{Q \times 10^3}{t_w h_w} = \checkmark \neq q_{all}$$

$0.94 \text{ t/cm}^2$

# Design of MG

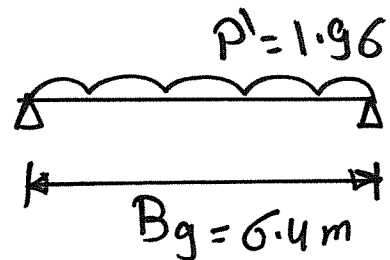


$$P = \frac{\delta_w h_1 + \delta_w H_g}{2} * H_{1g} = \frac{(1 * 1.85) + (1 * 3.9)}{2} * 2.05$$

$$P = 5.89 \text{ t/m'}$$

$$P' = \frac{P}{N_{MG}} = \frac{5.89}{3} = 1.96 \text{ t/m'}$$

$$M = \frac{P' * B_g^2}{8} = \frac{1.96 * 6.4^2}{8} = 10.03 \text{ t.m}$$



$$Q = \frac{P' * B_g}{2} = \frac{1.96 * 6.4}{2} = 6.272 \text{ ton}$$

$$\therefore Z_{req} = \frac{M \times 10^5}{1000} = \frac{10.03 \times 10^5}{1000} = 1003 \text{ cm}^3$$

Use S I B No = v v

Check of shear

$$q = \frac{Q \times 10^3}{t_w \times h_w} \neq q_{\text{all}} \quad 0.94 \text{ t/cm}^2$$

Design of roller

$$\frac{P_T \times 10^3}{N_r} = k \times D \times L$$

assume  $D = 20 \text{ cm}$  (  $L = 10 \text{ cm}$   $k = 117$

$$P_T = P \times B_g = 5.89 \times 6.4 = 37.696 \text{ ton}$$

$$\frac{37.696 \times 10^3}{N_r} = 117 \times \underset{20 \text{ cm}}{D} \times \underset{10 \text{ cm}}{L}$$

$$\therefore N_r = 1.6 \text{ roller}$$

$\therefore$  Used 6 roller



\* Force to required Lifting gate :

$$T = (G + \mu P_T + T_{\text{seal}}) \times F.O.S$$

$$G = g \times A_g$$

$$g = 0.06 \times S = 0.06 \times 6 = 0.36$$

$$A_g = B_g \times H_g = 6.4 \times 2.05 = 13.12 \text{ m}^2$$

$$\therefore G = 13.12 \times 0.36 = 4.72 \text{ ton}$$

$$P_T = 37.696 \text{ ton}$$

$$\mu = 0.1 \text{ (with roller)}$$

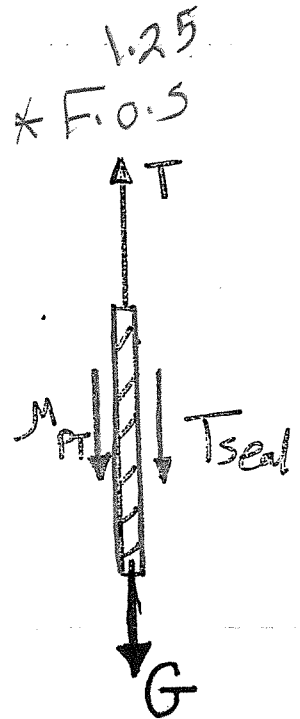
$$T_{\text{seal}} = 2 \times f \times b \times H_g \times P_{\text{av}}$$

$$= 2 \times 0.3 \times 0.2 \times 2.05 \times \left( \frac{(1 \times 1.85) + (1 \times 3.9)}{2} \right)$$

$$T_{\text{seal}} = 0.707 \text{ ton}$$

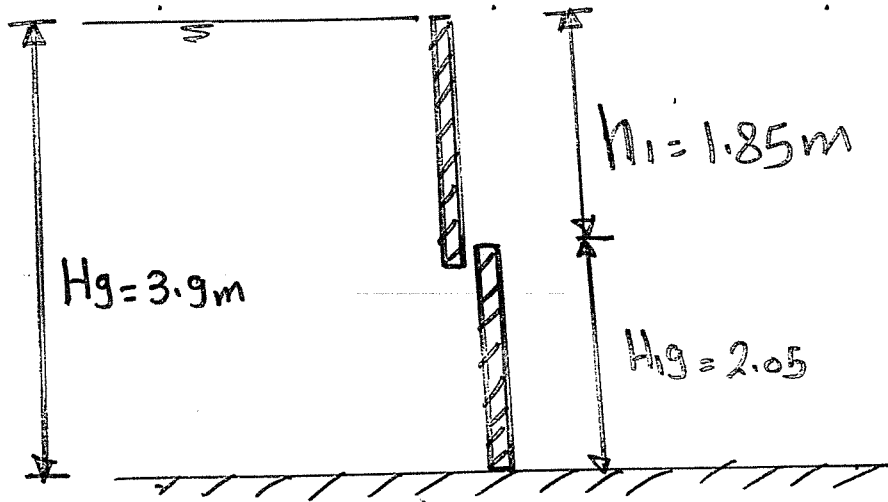
$$T = (4.72 + 0.1 \times 37.696 + 0.707)$$

$$T = 9.19 \text{ ton} \times 1.25$$



# Design the gate lifting structure

البوابة Double Gate ← تتجه تصريفها في اقل المثال.



$$H_g = y_{us} + 0.3$$

$$y_{us} = y_{Ds} + 0.1 = 3.5 + 0.1 = 3.6 \text{ m}$$

$$H_g = 3.6 + 0.3 = 3.9 \text{ m}$$

$$H_{1g} = \frac{H_g}{2} + 0.1 = \frac{3.9}{2} + 0.1 = 2.05 \text{ m}$$

$$B_g = S + 0.4 = 6.4 \text{ m}$$

## نبدأ في تصميم مكونات البوابة

□ Crane :-

$$\therefore S = 6m > 4m \text{ Use } 6 \text{ wheel}$$

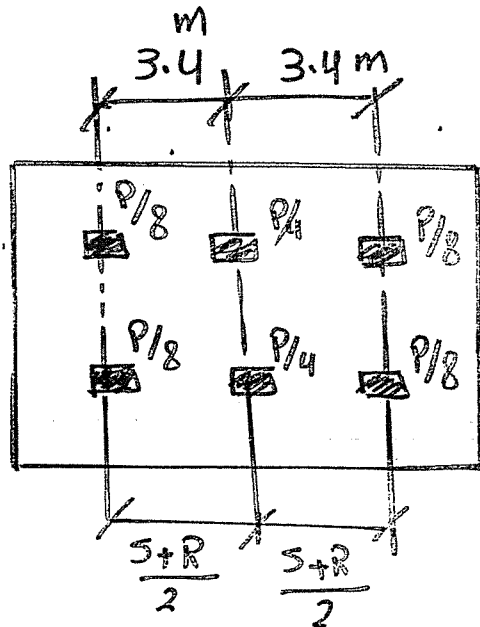
$$\therefore P = S \text{ ton}$$

$$\rightarrow P = 6 \text{ ton}$$

$$\rightarrow I = 20\% \text{ Impact}$$

$$\rightarrow F_L = \frac{P}{4} = \frac{6}{4} \text{ ton} = 1.5 \text{ ton} \text{ القوة الجانبية}$$

$$\rightarrow F_B = \frac{P}{7} = \frac{6}{7} \text{ ton} = 0.857 \text{ ton} \text{ قوة الفرامل}$$



Assume  $R = \frac{S}{5 \rightarrow 8} = \frac{6}{5 \rightarrow 8} = (1.2 - 0.75)$

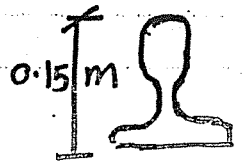
Pier ← عرض الـ

For R.C

Take  $(R = 0.8 \text{ m})$

## Rail

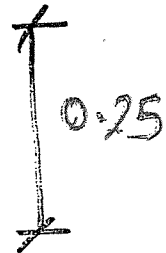
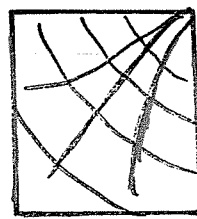
$$\text{own wt} = 0.05 \text{ t/m}^1$$



$$\text{height} = 0.15 \text{ m} = 15 \text{ cm}$$

## Sleeper

$$\gamma = 0.9 \text{ t/m}^3$$



$$\text{own wt} = (0.25 \times 0.25) \times 0.9$$

$$\text{own wt} = 0.056 \text{ t/m}^1$$

## Tie

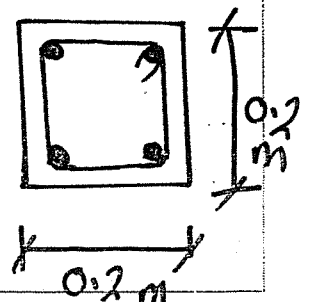
$$T = \frac{FL}{2} = \frac{P/4}{2} = \frac{S}{8} = \frac{6}{8} = 0.75 \text{ ton}$$

$$T_0 = T * (F.o.S) = 0.75 * 4 = 3 \text{ ton}$$

## Design

$$A_s = \frac{T_0 \times 10^3}{f_s} = \frac{3 \times 10^3}{1200} = 2.5 \text{ cm}^2$$

$$A_s = 0.45 \phi 12 \rightarrow \text{Used } 4 \phi 12$$

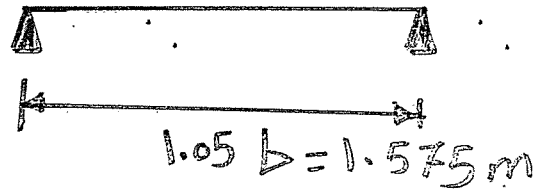


# Slot Channel

$$\text{at } S = 6 \text{ m}$$

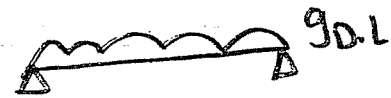
$$\therefore b = 1.5 \text{ m} \quad \text{جواب}$$

$$\therefore W = 0.9 \text{ m} \quad \text{جواب}$$



## Loading

a. Dead Load



$g.D.L.$  = own wt + Chaquor Plate

$$g.D.L. = 0.05 + 0.15 = 0.2 \text{ t/m}^2$$

$$M_{D.L.} = \frac{g.D.L. \times (1.05 b)^2}{8} = \frac{0.2 \times 1.575^2}{8}$$

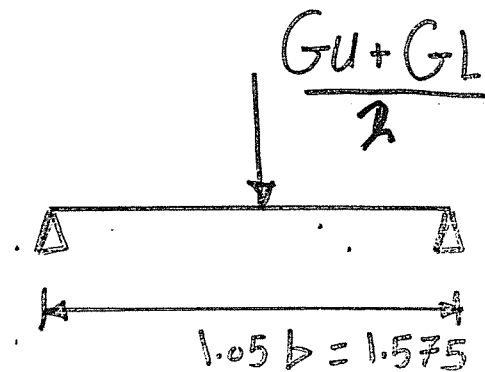
$$M_{D.L.} = 0.046 \text{ t.m}$$

$$Q_{D.L.} = \frac{g.D.L. \times (1.05 b)}{2} = \frac{0.2 \times 1.575}{2}$$

$$Q_{D.L.} = 0.118 \text{ ton}$$

b. Live Load :-

$$G_U = G_L$$

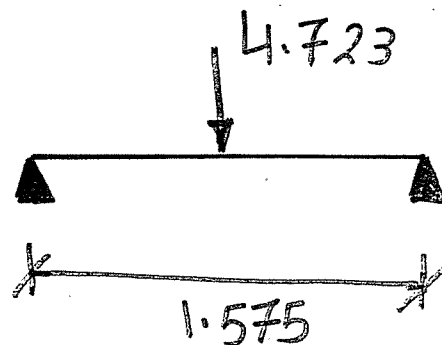


$$G_U = A_g * q$$

$$q = 0.06 * S = 0.06 * 6 = 0.36 \rightarrow S > 5m$$

$$A_g = H_g * B_g = 2.05 * 6.4 = 13.12 \text{ m}^2$$

$$G_U = G_L = 13.12 * 0.36 = 4.723 \text{ ton}$$



$$M_{L.L} = \frac{4.723 * 1.575}{4} = 1.86 \text{ t.m}$$

$$Q_{L.L} = \frac{4.723}{2} = 2.36 \text{ ton}$$

$$M_t = M_{D.L} + M_{L.L}$$

$$M_t = 0.046 + 1.86 = 1.906 \text{ ton.m}$$

$$Q_t = Q_{D.L} + Q_{L.L}$$

$$Q_t = 0.118 + 2.36 = 2.478 \text{ ton}$$

Design

$$Z_{2E} = \frac{M_t \times 10^5}{f_s \cdot 1200} = \frac{1.906 \times 10^5}{1200} = 159 \text{ cm}^3$$

$$Z_{1E} = \frac{Z_{2E}}{2} = \frac{159}{2} = 79.5 \text{ cm}^3$$

تبع اختيار الفلج من جدول ال steel (UPN)

Check of shear

$$q_r = \frac{Q_t \times 10^3}{2 t_w \times h_w} = \dots \neq q_{\text{all}}$$